


Welcome to



Energy Production Systems Engineering

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USF UNIVERSITY OF SOUTH FLORIDA POLYTECHNIC

Session 6: Electrical Systems

Spring 2012

Session 6: Electrical Systems

- **Electrical Systems**

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Electrical Systems

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Electrical Systems

- Transformers
- Construction
- K-Factor
- Winding configuration

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Electrical Systems

- Transformers & Transformer protection – Oil filled transformer – dry type transformers
- High efficiency
- K rating – steal quality – core area to operate farther away from knee of saturation curve
- Harmonics – positive / negative / zero sequence Triplen harmonics

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Table 10-11 – Classes of transformer cooling systems

Class	Method of cooling
OA	Liquid-immersed, self-cooled
OA/FA	Liquid-immersed, self-cooled/forced-air-cooled
OA/FA/FA	Liquid-immersed, self-cooled/forced-air-cooled/forced-air-cooled
OA/FA/FOA	Liquid-immersed, self-cooled/forced-air-cooled/forced-liquid-cooled
OA/FOA/FOA	Liquid-immersed, self-cooled/forced-air-cooled/forced-liquid-cooled/forced-liquid-cooled
FOA	Liquid-immersed, forced-liquid-cooled with forced-air-cooled
FOW	Liquid-immersed, forced-liquid-cooled with forced-water-cooled
OW	Liquid-immersed, water-cooled
OW/A	Liquid-immersed, water-cooled/self-cooled

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Dry type transformer cooling systems.

AA	Dry-type,* ventilated self-cooled
AFA	Dry-type,* ventilated forced-air-cooled
AA/FA	Dry-type,* ventilated self-cooled/forced-air-cooled
ANV	Dry-type,* non-ventilated, self-cooled
GA	Dry-type,* sealed self-cooled

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Voltage designations

Table 10-12(b)—Designation of voltage ratings of three-phase windings (schematic representation)

Identification	Nomenclature	Nominate marking	Typical winding diagram	Condensed usage guide
(2)(a)	E	2400		E shall indicate a winding of E volts which is suitable for A connection on an E volt system.
(2)(b)	E ₁ Y	4160Y		E ₁ Y shall indicate a winding of E volts which is suitable for A connection on an E volt system or for Y connection on an E ₁ volt system.

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Transformer K factor

Defined in UL 1561

I_h = rms current value (pu) at harmonic h

Harmonic currents = additional heating

K-factor X_{fmr} > K-factor System

$$K = \sum_{h=1}^{h=h_{max}} I_h^2 \cdot h^2$$

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Recommended K factor for various applications

TYPICAL LOAD K-FACTORS	
Electric discharge lighting	K-4
UPS with input filtering	K-4
Welders	K-4
Induction heating	K-4
PLCs / SS controls (other than VFDs)	K-4
Telecommunications equipment	K-13
UPS without input filtering	K-13
Multiwire receptacle circuits in general care areas Health care facilities and classrooms of schools, etc.	K-13
Multiwire receptacle circuits supplying inspection or testing equipment on an assembly or production line	K-13
Mainframe computer loads	K-20
Solid state motor drives (variable speed drives)	K-20
Multiwire receptacle circuits in critical care areas And operating/recovery rooms of hospitals	K-20

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Magnetization current / over excitation.

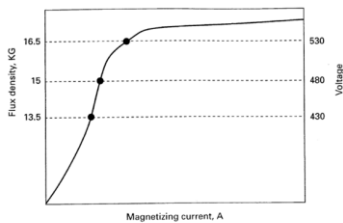


FIGURE 4.2.1 Magnetizing current in amperes.

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Transformer connections

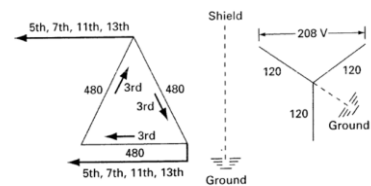


FIGURE 4.2.2 Schematic of delta-ye winding with electrostatic shield.

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TENV dry transformers in dirty, dusty environment – also cast epoxy vs. VPI

Auto transformer – smaller adjust voltage – no isolation

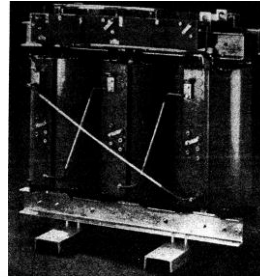
Reactor – current limiting – reduced voltage start – with capacitor for tuned filter

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Dry type – epoxy cast coil

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Instrument transformer – PT & CT

Transformer polarity

PT vs. CT defined by application

PT circuits in parallel – CT circuits in series

Do not short PT circuit – Do not open CT circuit
Special shorting switch

120V / 5A (1A)

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Accuracy – XYYZZZ

XX = max error at conditions

Y = C or T (calculated or tested)

ZZZ = volts secondary at 20X rated secondary current.

Example 7:

What is the max error at what voltage secondary for a;

10C200 current transformer

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10C200 current transformer

Maximum error of 10% at 200 Volts on secondary side at 20 times current (100A for 5A secondary)

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Table 10-7—Standard accuracy class ratings* current transformers in metal-clad switchgear

Ratio	Metering accuracy 60 Hz standard burdens					Relaying accuracy
	B 0.1	B 0.2	B 0.5	B 1.0	B 2.0	
50:5†	1.2	2.4‡	—	—	—	C or T 10
75:5†	1.2	2.4‡	—	—	—	C or T 10
100:5	1.2	2.4‡	—	—	—	C or T 10
150:5	0.6	1.2	2.4‡	—	—	C or T 20
200:5	0.6	1.2	2.4‡	—	—	C or T 20
300:5	0.6	1.2	2.4‡	2.4‡	—	C or T 20
400:5	0.3	0.6	1.2	1.2	2.4‡	C or T 50

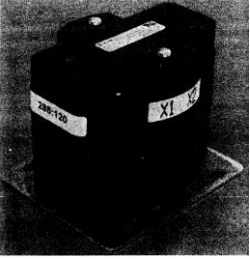
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Potential Transformer



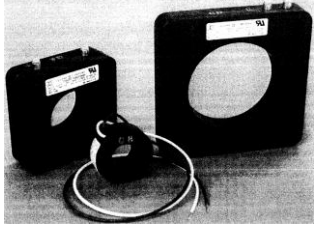
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Current Transformer



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Three parts of transformer –
Winding conductors, core material, insulation
Grain steel – M number (lower is lower loss)

Neutral terminal / conductor = twice size phase – maintain neutral to gnd voltage < 1 V. (solid grounded system)

Arrester 5 ft from transformer (vacuum switches and/or lighting exposure)

BIL ratings of transformers

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Insulation Test

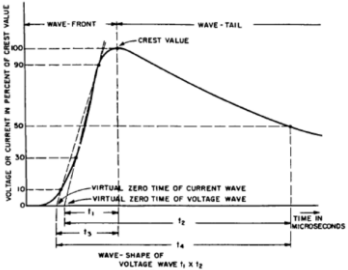
1 min, power-frequency high pot Test
1.2/50 full-wave voltage impulse test

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Full Wave vs. Chopped Wave test

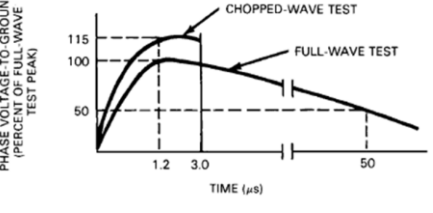


Figure 6-12—Standard impulse test waves

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Insulation class and nominal lightning rating	Winding								Bushing withstand voltages					
	BIL per test		Chopped wave		BIL full wave (1.2/50)		Switching surge level		60-cycle 1 min dry		60-cycle 10 s wet		BIL impulse full wave (1.2/50)	
	kV (rms)	kV (crest)	kV (crest)	µs	kV (crest)	kV (crest)	kV (crest)	kV (crest)	kV (rms)	kV (crest)	kV (rms)	kV (crest)	kV (crest)	kV (crest)
1.2	10	54 (50)	1.5 (1)	45 (30)	20	15 (10)	13 (9)	45 (30)						
2.5	15	69 (54)	1.5 (1.25)	60 (45)	35	21 (15)	20 (13)	60 (45)						
5.0	30	138 (99)	1.6 (1.5)	75 (60)	50	27 (21)	24 (20)	75 (60)						
8.7	30	110 (80)	1.8 (1.6)	95 (70)	55	35 (27)	30 (24)	95 (70)						
15.0	34	130 (110)	2.0 (1.8)	110 (90)	75	50 (35)	45 (30)	110 (90)						
25.0	30	175	3.0	150	100	70	70 (60)	150						
34.5	30	230	3.0	200	140	95	95	200						
46.0	95	290	3.0	250	190	120	120	250						
69.0	140	400	3.0	300	280	175	175	350						
92.0	185	520	3.0	450	375	225	190	450						
115.0	230	630	3.0	500	400	280	230	550						
138.0	275	750	3.0	650	540	335	275	650						
161.0	325	865	3.0	750	620	385	315	750						

NOTE—Values in parentheses are for distribution transformers, instrument transformers, excitation transformers, dry- and induction-voltage regulators, and other products for distribution systems. The winding surge levels shown are applicable only to power transformers (not distribution transformers). Test voltages are defined in IEEE Std C57.12.00-1990.



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Table 6-3—Impulse test levels for dry-type transformers

Nominal winding voltage (volts)	Grounded wye	High-potential test	
		kV (rms)	kV (crest)
Delta or ungrounded wye	1200Y/693	4	10
		4	10
2520	4360Y/2520	10	20
4160-7200	8720Y/5040	12	30
		10	30
8320		19	45
12 000-13 800	13 800Y/7970	31	60
		10	60
18 000	22 860Y/13 200	34	95
		10	95
23 000	24 940Y/14 400	37	110
		10	110
27 600	34 500Y/19 920	40	125
		10	125
34 500		50	150

NOTE—Data from IEEE Std C57.12.01-1979. Nominal voltages shown are exactly as tabulated in IEEE Std C57.12.01-1979 and are not, in all cases, in accordance with the classifications commonly encountered on industrial and commercial systems.



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Dry Type transformer BIL

Nominal system voltage (kV)	Basic lightning impulse insulation levels (BILs) in common use (kV crest)									
	10	20	30	45	60	95	110	125	150	200
1.2	S	1	1							
2.5		S	1	1						
5.0			S	1	1					
8.7				S	1	1				
15.0					S	1	1			
25.0						2	S	1	1	
34.5								2	S	1



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Standard impedance < 500KVA = 3-5 %
>500 KVA = 5.75 %

Fan cooling dry type = 133% rating w/ fan

Caution, temperature of conductor connection

VPI – vacuum to draw moisture out, inject epoxy, pressure applied (inert gas) to push epoxy into winding – heat to cure epoxy



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Electrical Systems

Thermal insulation class (AMB 30C)

AVG TMP RISE C	HOT SPOT DIFF C	HIGHEST PERM RISE C	CLASS
55	10	105	A105
65	15	120	A120
80	30	150	B150
115	30	185	F185
150	30	220	H220



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- NEMA 1
- NEMA 3R
- NEMA 4
- NEMA 12

Dry type reduced environmental requirements and fire protection compared with oil

Dry type available to about 15MVA



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Electrical Systems

Circuit Breaker – switch to open under current

- Driven by spring action both close and trip
- DC power for charging motor
- External relay trip on protection
- Arc drawn –
- Air / Vacuum / SF6 / Oil
- Coordination – discussed later in relaying section

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Table 6-2—Basic impulse insulation levels (BILs) of power circuit breakers, switchgear assemblies, and metal-enclosed buses

Voltage rating (kV)	BIL (kv)	Voltage rating (kV)	BIL (kV)	Voltage rating (kV)	BIL (kV)
2.4	45	23	150	115	550
4.16	60	34.5	200	138	650
7.2	75*	46	250	161	750
13.8	95	69	350	230	900
14.4	110	92	450	345	1300

*95 for metal-clad switchgear with power circuit breakers

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- Special considerations:
- Need DC to trip / close – battery fed
- Synchronizing
- Dead bus transfer
- Motor bus transfer – reclosing

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Grounding –
Ungrounded / low impedance / high impedance / solid grounded

Advantages / disadvantages

- Ungrounded – reliable – first GF no trip
- High transient voltage
- Difficult to locate ground
- Ground detection via open delta transformer (DRAW)

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Electrical Systems

Grounding –
 High impedance ground (10A) – low damage, can alarm on ground increase reliability,
 Need sensitive relay to detect and locate ground
 Transient less than ungrounded but higher than low impedance ground.

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Electrical Systems

Grounding –
 Low impedance ground (400A) – easily detected, higher damage, easily located, transients less, trip on fault, reduced security

Solid grounded – most damage, easily detected, easily located, transients minimum, trip on fault, reduced security

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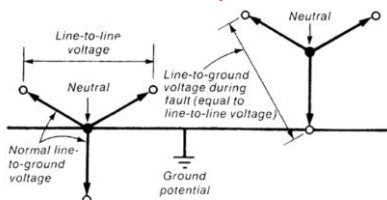


FIGURE 4.3.2 No fault versus ground fault for a three-phase power system.

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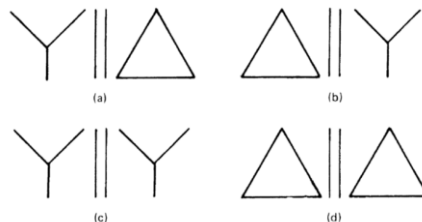


FIGURE 4.3.3 Transformers may be connected (a) wye-delta, (b) delta-wye, (c) wye-wye, and (d) delta-delta.

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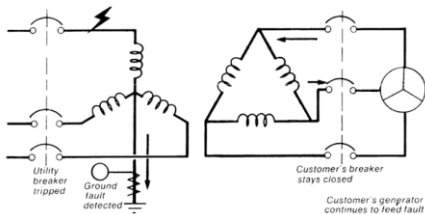


FIGURE 4.3.4 Wye-delta connection is best for most installations, but if the customer's generator is large, it may continue to feed a fault on the utility side of the transformer.

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Differential protection on delta wye may need wye delta connected CTs to compensate for 30 degree phase shift.

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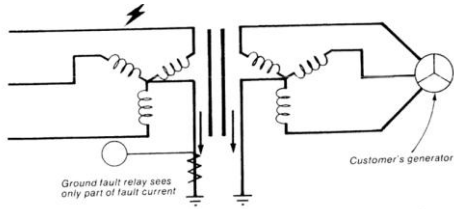


FIGURE 4.3.5 Wye-wye connection is least desirable because ground fault current is divided between two grounding legs.

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Can add grounding transformer to ground a delta fed system

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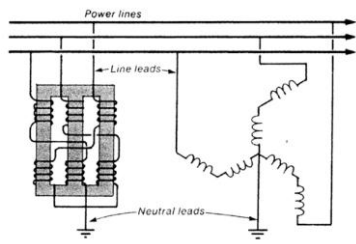


FIGURE 4.3.7 Zigzag grounding transformer has primary and secondary windings connected as shown, with the secondary neutral point grounded.

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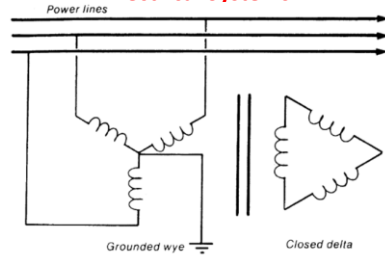


FIGURE 4.3.6 Any transformer will double as a grounding device if its primary is wye-connected and its secondary is a closed delta.

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System-grounding design considerations –
Three levels of conductor insulation for MV cables: 100, 133, and 173% levels.
The solidly grounded system permits the use of 100% insulation level.
If fault cleared within 1 hour, 133% insulation level should be specified
If fault cleared more than 1 hour, 173% voltage level insulation should be used

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Grounding –
Adequate ground-return conductors to minimize the inherent **step-and-touch potentials** w/ solidly grounded systems
Instantaneous ground fault relaying to minimize the fault duration.

See the NEC NESC and IEEE Std 80

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All non-current-carrying metallic structures are interconnected and grounded.

Purpose:

- Minimize potential difference between metallic members
- Minimizing the risk of electric shocks to personnel
- Improve protective device performance
- d) To avoid fires in combustible atmospheres

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Inductance of ground path

$$L = 4 \times 10^{-7} \ln(D/r') \quad H/m$$

Therefore, L increases as D increases

**VD increases as D increases &
Current tends to flow in closest cond.**

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Two or more rods suggested

Distance between rods must be $Lr1 + Lr2$

Example two 8 ft rods, should be 16ft distance

(Numerous books and articles show the distance between two standard length 8 or 10 ft rods to be 3 m (10 ft), which is incorrect.)

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Impedance depended on IEEE 80 Calc.

Larger substations and generating stations $< 1\Omega$

Smaller substations and for industrial plants $< 5\Omega$

NEC, Article 250, approves the use of a single electrode, if $< 25\Omega$

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Protective relaying & coordination:

Two functions – Protection of equipment (secondary)
Security of system (primary)

Trip when faulty condition present AND don't trip when faulty condition not present

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Balance of following concepts:

Reliability – Relay system trip when fault exists in protective zone

Security – Relay system trip only when fault exists in protective zone

Selectivity – Relay system should trip minimum equipment to remove fault

Speed – Relay system remove fault fast to minimize damage and arc flash incident energy.

Simplicity – minimum amount of equipment – maximize reliability

Economics – Reasonable cost

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Electrical Systems

Most common – 50, 51, 27, 59, 81O, 81U, 87

PTs and CTs feed relays

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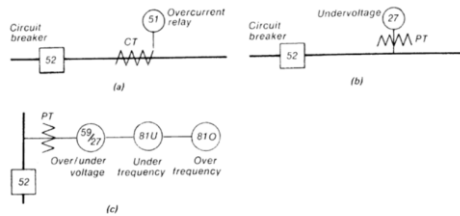


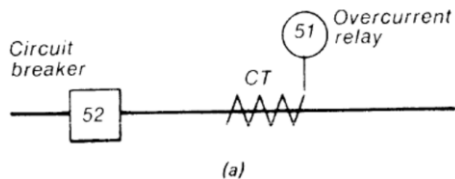
FIGURE 4.3.10 Instrument transformers may be (a) current (CT) or (b, c) potential (PT).

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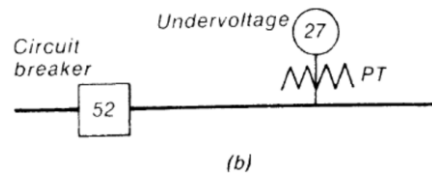


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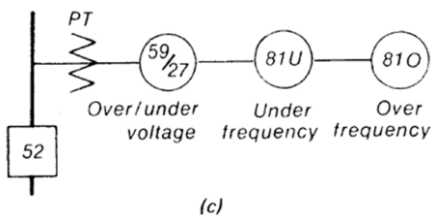


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Ground fault –
Unbalanced current – not easily detected by phase relay,
use sensitive ground fault relay
For grounded system, use 50G or 51G as shown below. For
ungrounded system use broken delta with 59 relay.

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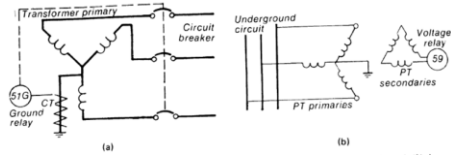


FIGURE 4.3.11 Ground fault (a) on one phase of a grounded three-phase circuit and (b) in an ungrounded circuit.

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Phase Faults:
Line to Line, Line to Ground (solid system), and 3 phase fault detection. 50 and/or 51 detect.

Overvoltage (59) – typically used on neutral or ground detection systems

Frequency (81O & 81U) – indication of system transient. Protection during “Islanding”

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Differential relay (87) –
Detect internal fault quickly – ignore external fault reliably
May be more than just 2 winding device (i.e. 6 CT inputs)

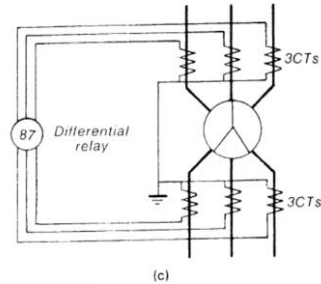
Overcurrent (50/51) both phase and ground detection – 51 device to allow for coordination between elements

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Electrical Systems



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Directional overcurrent (67) –
Control flow of power – prevent motoring of generator
Need VT & CT to polarize relay

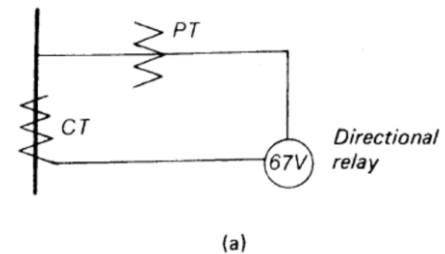
Distance relay (21), trip if fault in zone 1, backup for zone 2, 3. Needs VT & CT input. Common application is looking back into generator impedance (quick trip of breaker for gen fault).

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Synchronizing relay (25) -

Both Synchronizing and Synch check

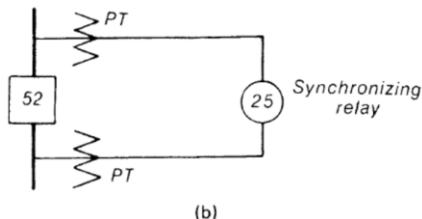
Magnitude, angle, rotation, frequency

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(b)

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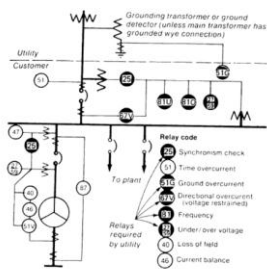


FIGURE 4.3.13 Basic protection scheme suggested by Southern California Edison Co. for total generation greater than 200 kVA. (Courtesy Southern California Edison Co.)

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Electrical Systems

Typical Relay & Protection One-line Diagram

Electrical Systems

Short Circuit Current Calculations

Purpose

- Present considerations of short-circuit current calculations;
- Illustrate common methods for calculations;
- Furnish typical data used in calculations.

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Rotating Machine Equivalent Circuit

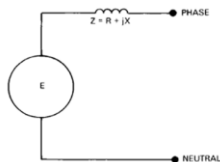


Figure 4-1—Equivalent circuit for generators and motors
E = (driving voltage, X varies with time)

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Electrical Systems

- X_d'' - subtransient reactance – (0 < t < 0.1s)
- X_d' - transient reactance – (0.1 < t < 0.5 to 2.0s)
- X_d - synchronous reactance – (0.5 to 2.0s < t) Steady State

When given X_{dv}'' – (at rated voltage, saturated, smaller) and X_{di}'' – (at rated current unsaturated, larger), use X_{dv}''

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Electrical Systems

X_d'' - subtransient reactance – ($0 < t < 0.1s$)
 No Value for X_d' and X_d as motor only contributes SCA for initial cycles.



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Electrical Systems

Utility normally shown with as infinite bus with fixed impedance.
 For MV & HV systems, R usually ignored
 For LV system R included
 Arc Resistance not zero



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Electrical Systems

Select location for purpose of calculation
 - Establish simple model
 Recognize restraints of model
 Adjust model if assumptions too restraining



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Electrical Systems

Step 1: Prepare system diagrams
 Step 2: Collect and convert impedance data
 Step 3: Combine impedances
 Step 4: Calculate short-circuit current



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Electrical Systems

Wye Delta Conversion

$$A = \frac{b \cdot c}{a} + b + c$$

$$B = \frac{a \cdot c}{b} + a + c$$

$$C = \frac{a \cdot b}{c} + a + b$$



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Electrical Systems

Delta Wye Conversion

$$a = \frac{B \cdot C}{A + B + C}$$

$$b = \frac{A \cdot C}{A + B + C}$$

$$c = \frac{A \cdot B}{A + B + C}$$



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Electrical Systems

Per Unit Calculations

$$\begin{aligned} \text{base current (amperes)} &= \frac{\text{base kVA (1000)}}{\sqrt{3} (\text{base V})} = \frac{\text{base kVA}}{\sqrt{3} (\text{base kV})} \\ &= \frac{\text{base MVA } 10^6}{\sqrt{3} (\text{base V})} = \frac{\text{base MVA (1000)}}{\sqrt{3} (\text{base kV})} \\ \text{base impedance (ohms)} &= \frac{\text{base V}}{\sqrt{3} (\text{base A})} = \frac{(\text{base V})^2}{\text{base kVA (1000)}} \\ &= \frac{(\text{base kV})^2(1000)}{\text{base kVA}} = \frac{(\text{base kV})^2}{\text{base MVA}} \end{aligned}$$

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Electrical Systems

Per Unit Calculations

$$\begin{aligned} Z_{pu} &= \frac{\text{actual impedance in ohms (base MVA)}}{(\text{base kV})^2} \\ &= \frac{\text{actual impedance in ohms (base kVA)}}{(\text{base kV})^2(1000)} \\ Z_{pu} &= \frac{\text{percent impedance (base kVA)}}{\text{kVA rating (100)}} \\ &= \frac{\text{percent impedance (10) (base MVA)}}{\text{kVA rating}} \end{aligned}$$

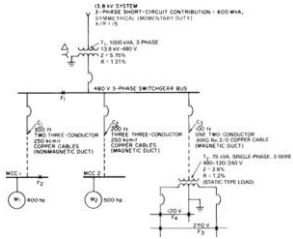
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Electrical Systems

example



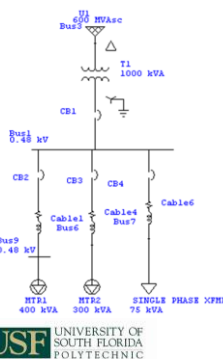
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Electrical Systems

Software Model



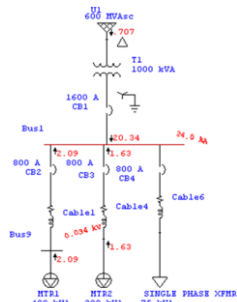
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Electrical Systems

Subtransient Result



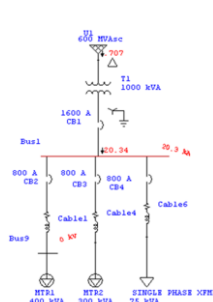
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Steady state result



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Electrical Systems

Fault at MCC1

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Correct Phase TCC

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Correct Ground TCC

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Incorrect Phase TCC

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Electrical Systems

In-Plant Electrical Distribution System

- Ensure reliability of system
- Either higher spinning reserve – high failure rate
- Low spinning reserve – low failure rate

Without reliable distribution system, plant operation can not be reliable.

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Electrical Systems

Distribution system design standards:

- IEEE Color Books
- EMERALD BOOK IEEE Std 1100-1999 IEEE Recommended Practice for Powering and Grounding Electronic Equipment
- RED BOOK IEEE Std 141-1993 IEEE Recommended Practice for Electric Power Distribution for Industrial Plants

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Distribution system design standards:
IEEE Color Books

GREEN BOOK IEEE Std 142-1991 IEEE Recommended
Practice for Grounding of Industrial and Commercial Power
Systems

BUFF BOOK IEEE Std 242-2001 IEEE Recommended
Practice for Protection and Coordination of Industrial and
Commercial Power Systems

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IEEE Color Books

BROWN BOOK IEEE Std 399-1997 IEEE Recommended
Practice for Industrial and Commercial Power Systems
Analysis

ORANGE BOOK IEEE Std 446-1995 IEEE Recommended
Practice for Emergency and Standby Power Systems for
Industrial and Commercial Applications

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IEEE Color Books

GOLD BOOK IEEE Std 493-1997 IEEE Recommended
Practice for the Design of Reliable Industrial and
Commercial Power Systems

BRONZE BOOK IEEE Std 739-1995 IEEE Recommended
Practice for Energy Management in Industrial and
Commercial Facilities

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NFPA HFPE and Society of Fire Protection Engineers SFPE
Handbook of Fire Protection Engineering
NFPA 101H, Life Safety Code Handbook
NFPA 20, Centrifugal Fire Pumps
NFPA 70, National Electrical Code
NFPA 70B, Electrical Equipment Maintenance
NFPA 70E, Electrical Safety Requirements for Employee
Workplaces
NFPA 72, National Fire Alarm Code
NFPA 75, Protection of Electronic Computer/Data
Processing Equipment

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Electrical Systems

Difference between
Code (Stand alone)
Standard (Shall)
Recommended Practice (Should)
Guide (May)

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Electrical Systems

System Planning.

- a) Load development & schedule
 - 1) Peak load requirements
 - 2) Temporary power
 - 3) Timing
- b) Load variations – load growth.

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Electrical Systems

- c) Nature of load in terms of its occurrence
- 1) Continuous
 - 2) Intermittent
 - 3) Cyclical
 - 4) Special or unusual loads
 - 5) Combination of above
- d) Expected power factor

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Electrical Systems

- Cost vs. Reliability
- Radial system
 - Primary-selective system
 - Secondary selective system
 - Simple spot network system
 - Secondary-network system

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Electrical Systems

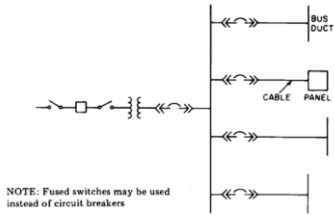


Figure 2-1—Simple radial system

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Electrical Systems

- Simple Radial System
- Fault in device = power outage
 - Maintenance difficult
- Operation simple
Low capital cost
Larger installations where outage time not critical

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Electrical Systems

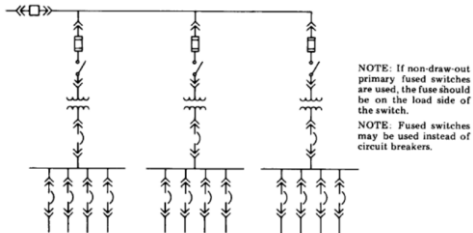


Figure 2-2—Expanded radial system

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Electrical Systems

- Expanded Radial System –
- Fault in main feed = power outage
 - Fault in xfmr = reduced outage
 - Maintenance difficult
- Operation simple
Low capital cost

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Electrical Systems

NOTE: If non-draw-out fused switches are used, the fuse should be on the load side of the switch.

NOTE: An alternate arrangement uses a primary selector switch with a single fused interrupter switch (which may not have certified current-switching ability).

Figure 2-3—Primary selective system 103

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Primary Selective System –

- Protection against loss of primary feed
- Still Xfmr Dependent
- Primary source Maintenance easier
- Slightly higher capital cost

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Electrical Systems

Figure 2-4—Primary loop system 105

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Protection against loss of primary feed

Still Xfmr Dependent

Slightly higher capital cost

Operation slightly more difficult

Open loop operation

More reliable with loop closed and directional protection

but two devices to isolate fault

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Electrical Systems

(a) Secondary selective system 107

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Electrical Systems

Protection against loss of primary feed and primary xfmr

Maintenance of xfmr

Higher capital cost

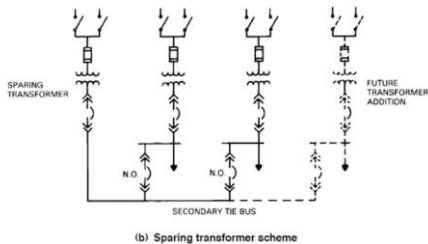
Operation more difficult

Size xfmr & breaker for full load

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Electrical Systems



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Electrical Systems

Similar to secondary selective system
Xfmr sized for only one bus
N+1 transformer needed
Operation difficult – interlock so xfmr only feed one bus at a time
Possible retrofit

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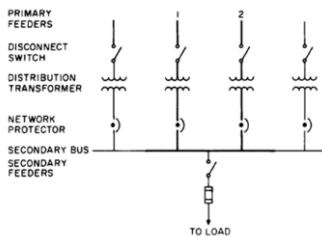


Figure 2-6—Secondary spot network

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Electrical Systems

Requires Network Protector
Trip on reverse power
High reliability
High cost

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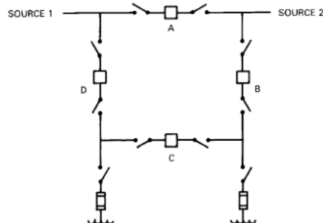


Figure 2-7—Ring bus system

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Two devices to isolate fault
Trip on reverse power
High reliability
Higher cost

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Electrical Systems

Expected daily and annual load factor:

$$\text{Daily } \frac{\text{kWh for 24 h/24 h}}{\text{peak kW during the 24 h}} = \frac{\text{avg. kW}}{\text{peak kW}}$$

$$\text{Annual } \frac{\text{kWh for 8670 h/8670 h}}{\text{peak kW during the 8670 h}} = \frac{\text{avg. kW}}{\text{peak kW}}$$

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Electrical Systems

Large motor-starting requirements

- 1) HP, FLA, LRA
- 2) synchronous - induction
- 3) Voltage
- 4) Starting requirements

Special or unusual loads such as

- 1) Welding
- 2) Induction heating or melting
- 3) Portable (Crane)

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Electrical Systems

Harmonic-generating loads

- 1) VFDs
- 2) Arc discharge lighting
- 3) Arc furnaces
- 4) SCR controlled loads

Special power quality requirements for sensitive or critical loads

- 1) Data processing operations
- 2) Special machines (Semiconductor process)
- 3) Continuous process loads

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To be continued ...



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End of Session 6:
Electrical Systems

Spring 2012